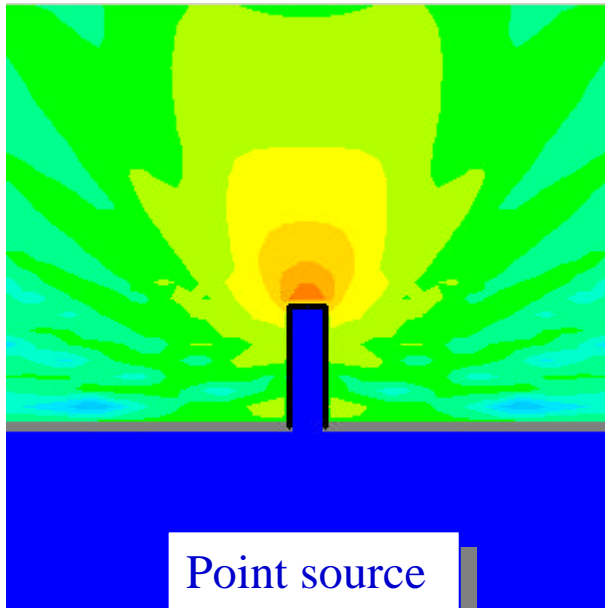


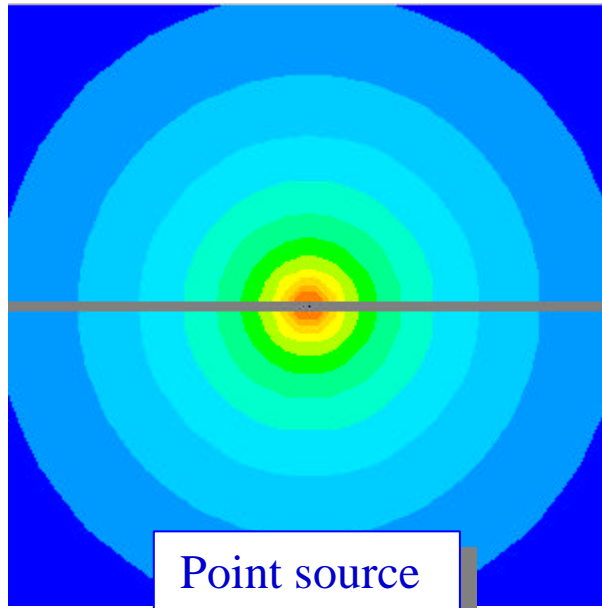
Radiation impedance of cones at high frequencies

- Radiation into free space
- Boundary element method
- Mechanical model
- Sound pressure measurements
- Approximation of radiation impedance

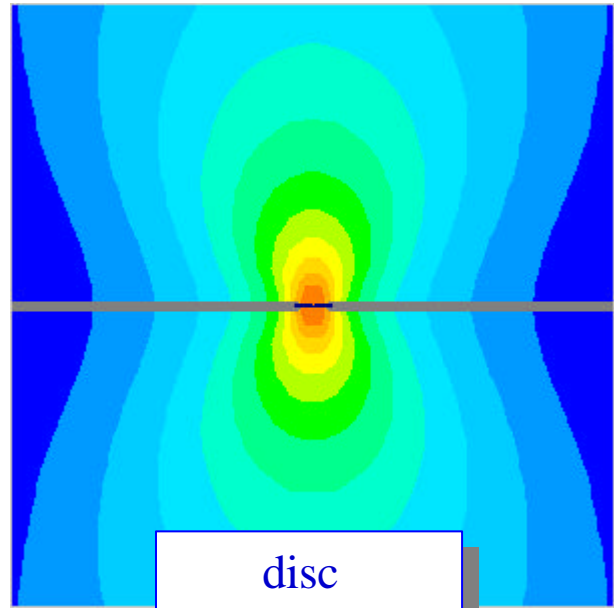
Radiation into free space



Point source
Finite baffle
1 kHz



Point source
Infinite baffle
1 kHz

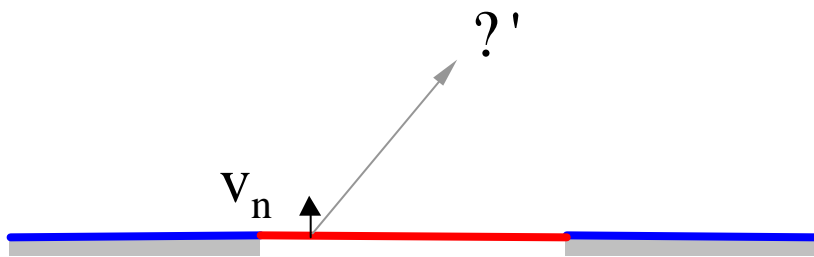


disc
Infinite baffle
1 kHz

Infinite baffle avoids
interferences caused by the
baffle

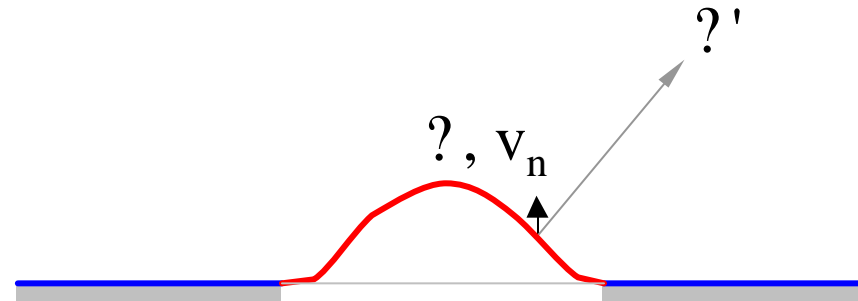
Boundary element method

Flat source:
Rayleigh's formula



$$f' = \int_S v_n G ds$$

Otherwise:
Helmholtz integral



$$f' = \int_S v_n G ds + \int_S f G_n ds$$

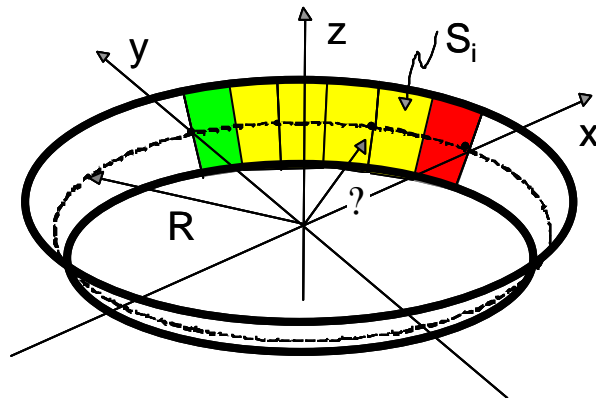
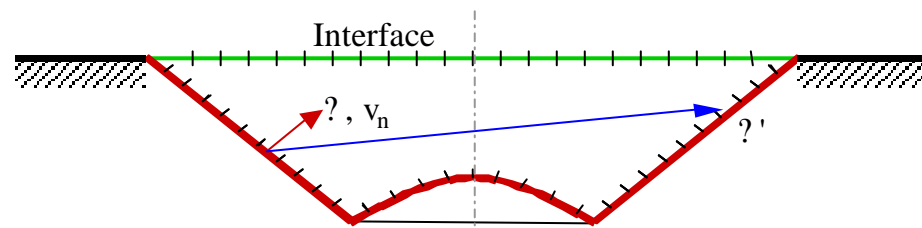
Unknown



Boundary element method

$$f' = \int_S v_n G \, ds - \int_S f G_n \, ds$$

Unknown \rightarrow



Solving Helmholtz Integral

Discretize surface into small segments (rings)

Lower receiving points of Helmholtz Integral onto surface segments

Assume constant potential across a segment

Integrate Green functions numerically for each ring

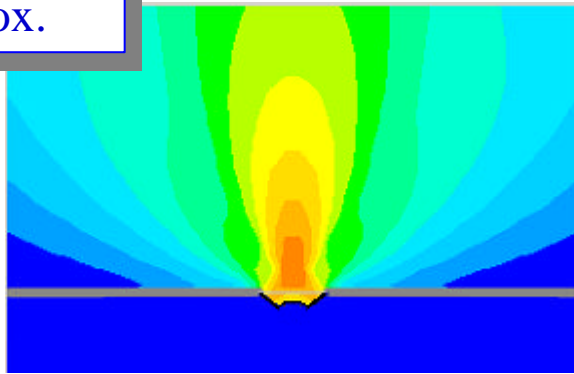
Solve linear equation system for surface potentials ?

Apply Helmholtz Integral again for any receiving point

Boundary element method

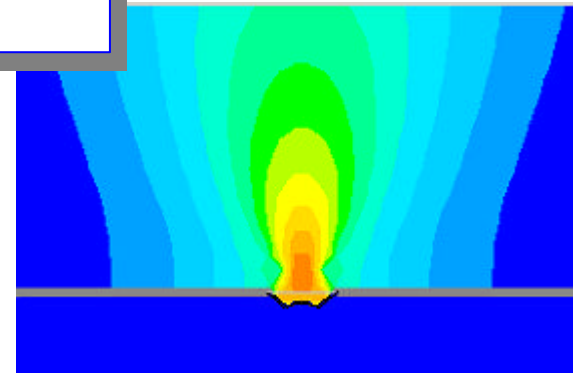
Rayleigh
formula
approx.

$$f' = \int_S v_n \rho G \, ds$$

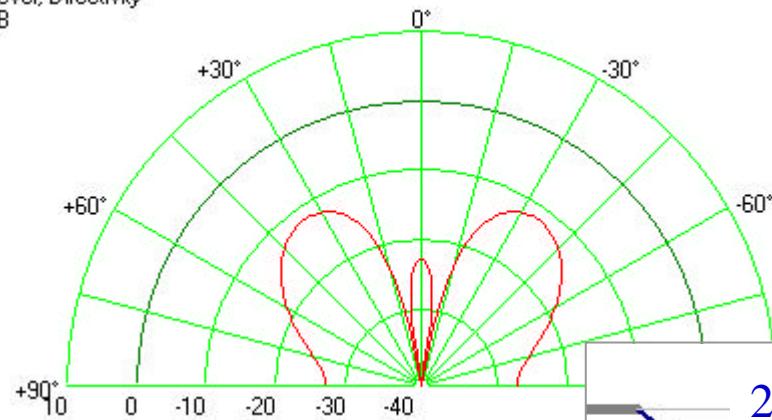


Helmholtz
Integral

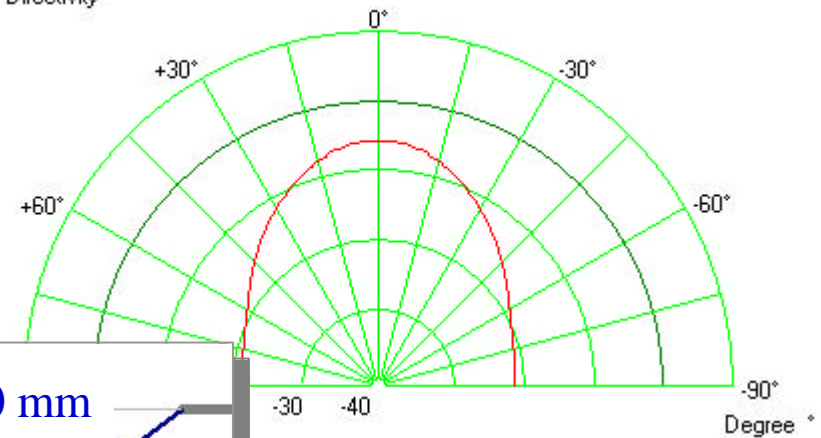
$$f' = \int_S v_n \rho G \, ds + \int_S f \rho G_n \, ds$$



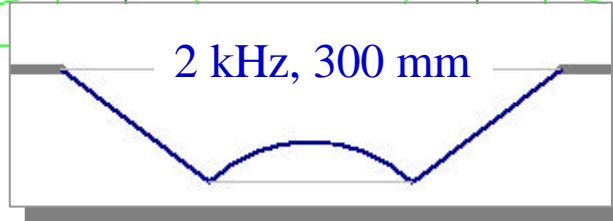
Level, Directivity
dB



Level, Directivity
dB



2 kHz, 300 mm



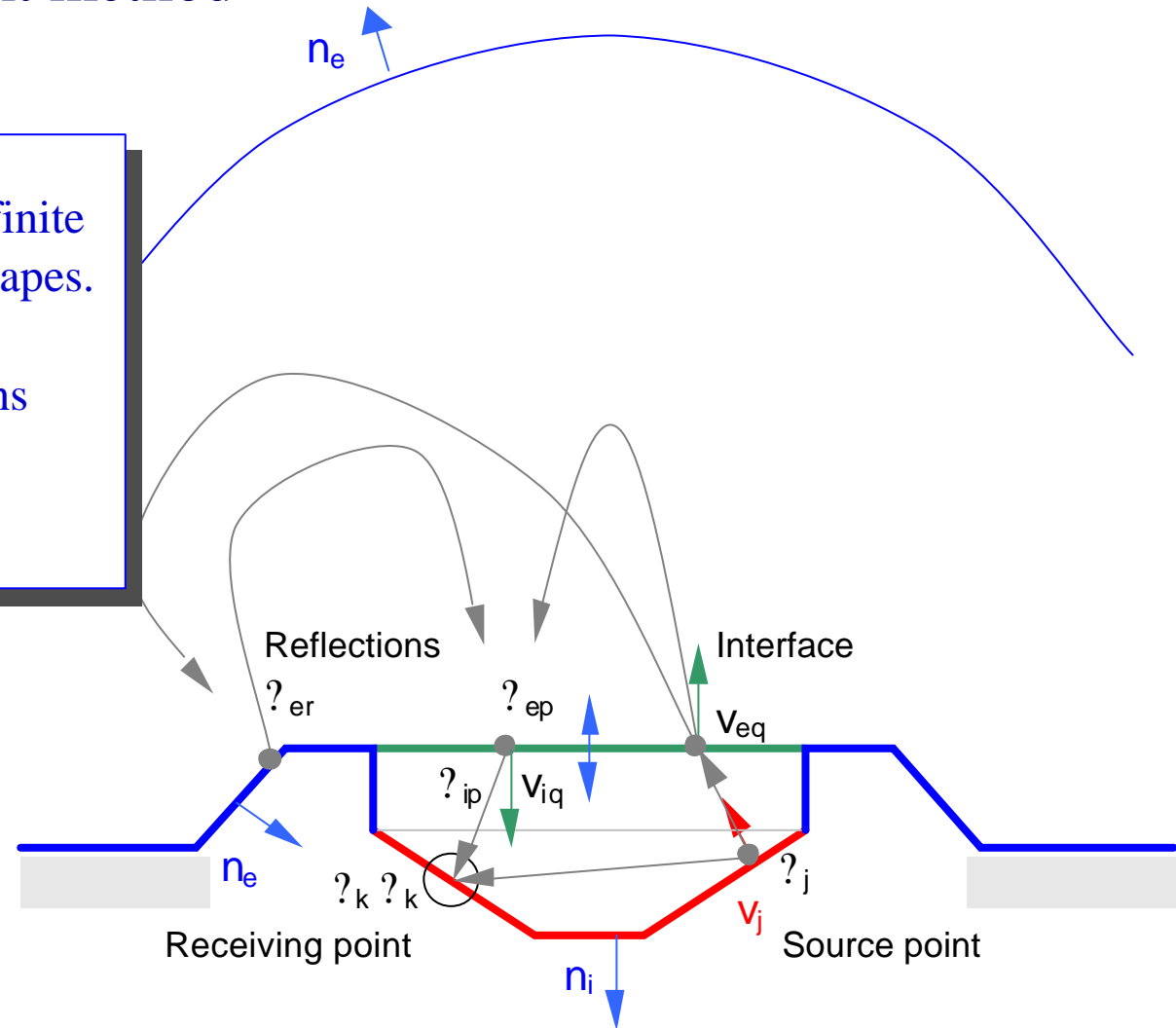
Boundary element method

Coupled BEM for infinite baffle and concave shapes.

Interface conditions

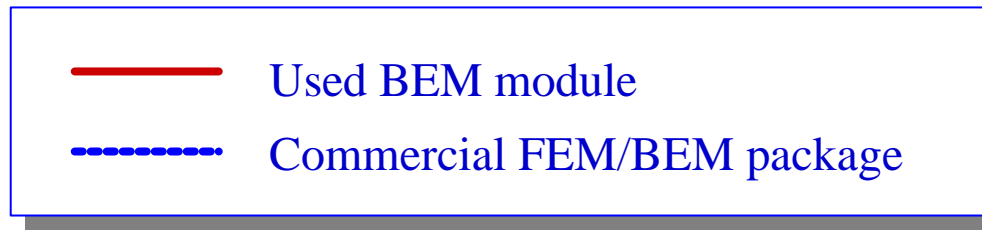
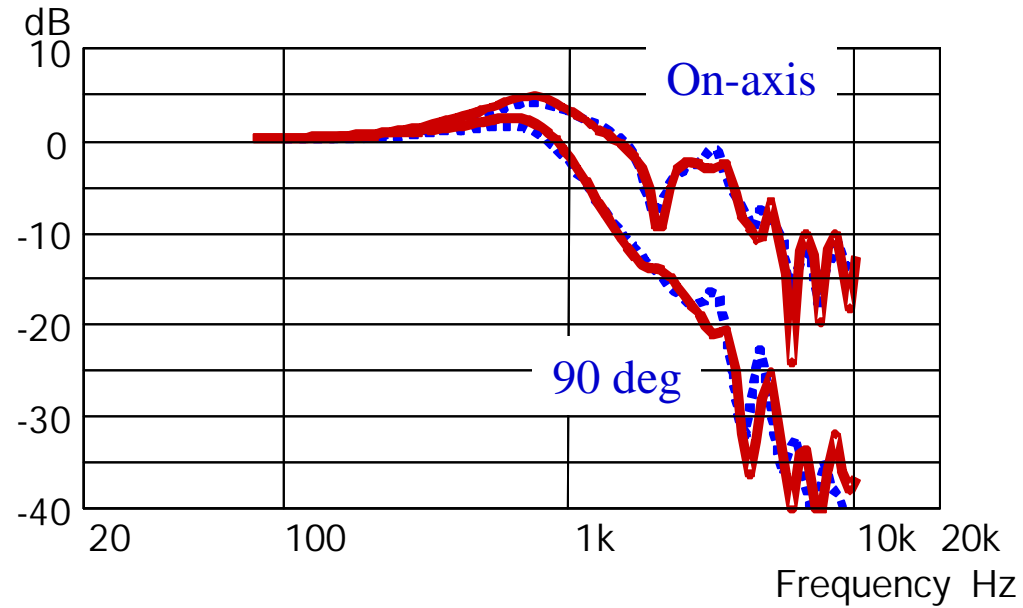
$$\phi_i = \phi_e$$

$$V_i = -V_e$$



Boundary element method

Sound pressure comparison

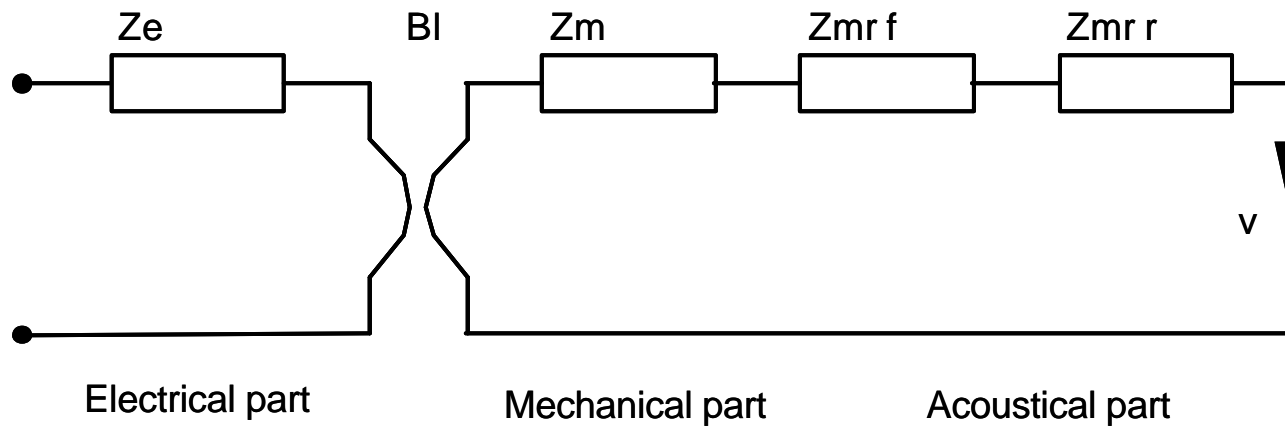


Mechanical Model

- BEM models radiation in great detail.
Arbitrary properties of each segment.
- Dynamics of membrane would be next natural step.
Bending wave radiation and coupling.
Interesting studies have been done before.
- Rigid body mode is investigated here only.
- Simulation bandwidth restricted to low and mid bands,
but BEM increases bandwidth by 1 ... 2 octaves against disc approximation.
- Only geometrical data are necessary, no material data

Mechanical Model

Rigid body model of electro-dynamical loudspeaker driver



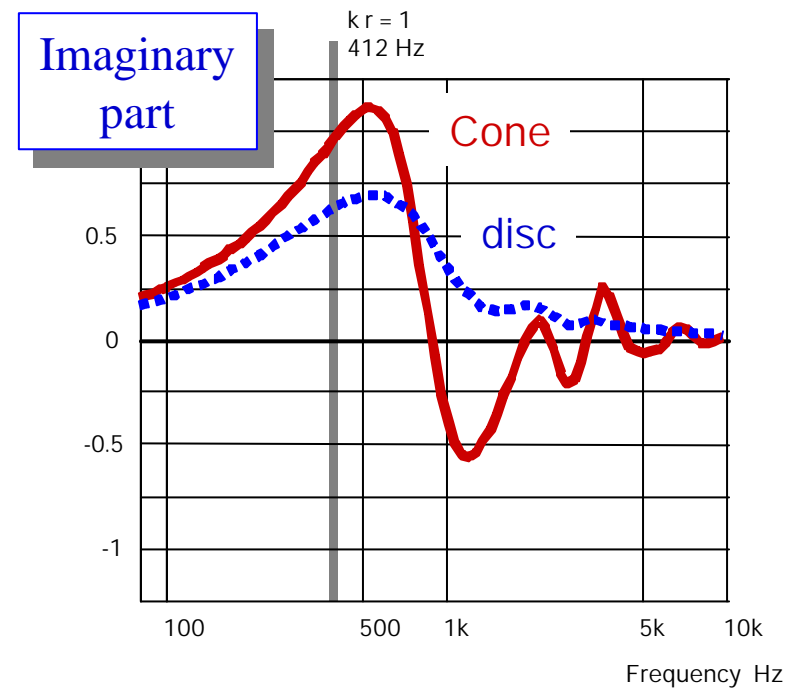
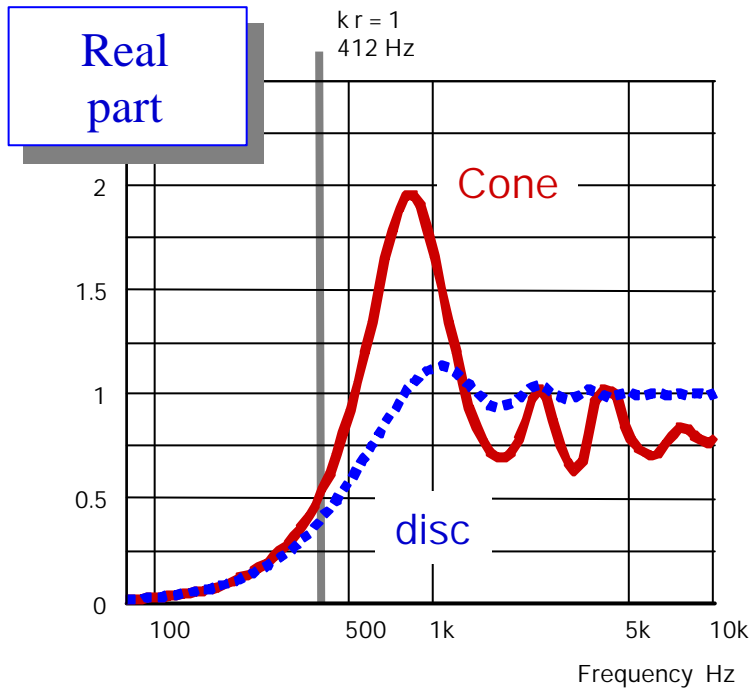
Radiation impedance

$$Z_{mr} \approx \frac{i \rho_0 c_0 S_d \cos^2 \alpha_i}{v}$$

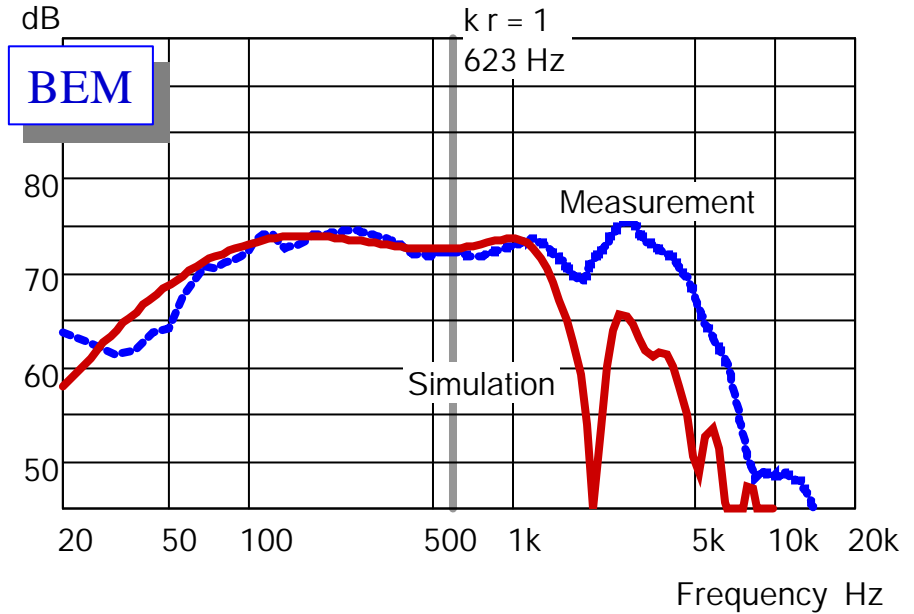
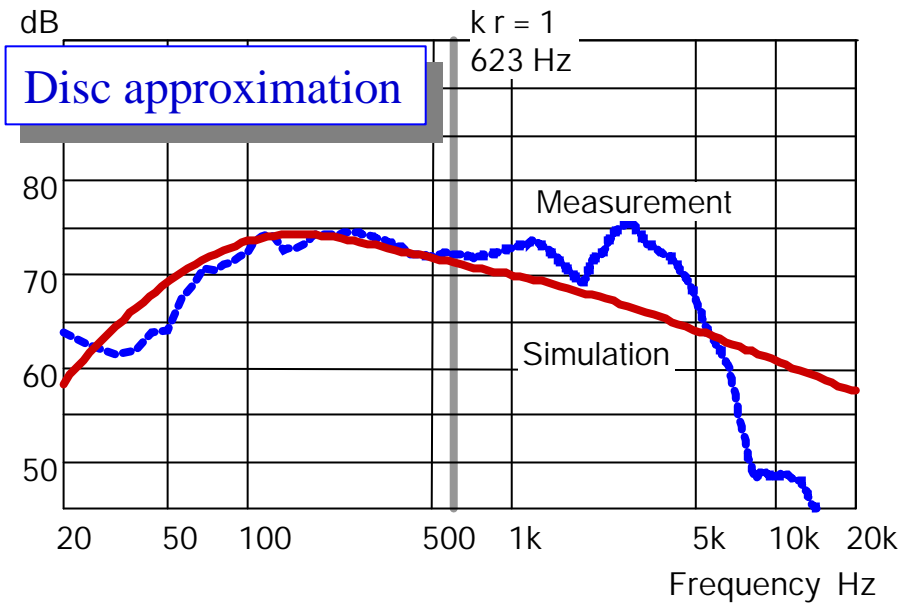
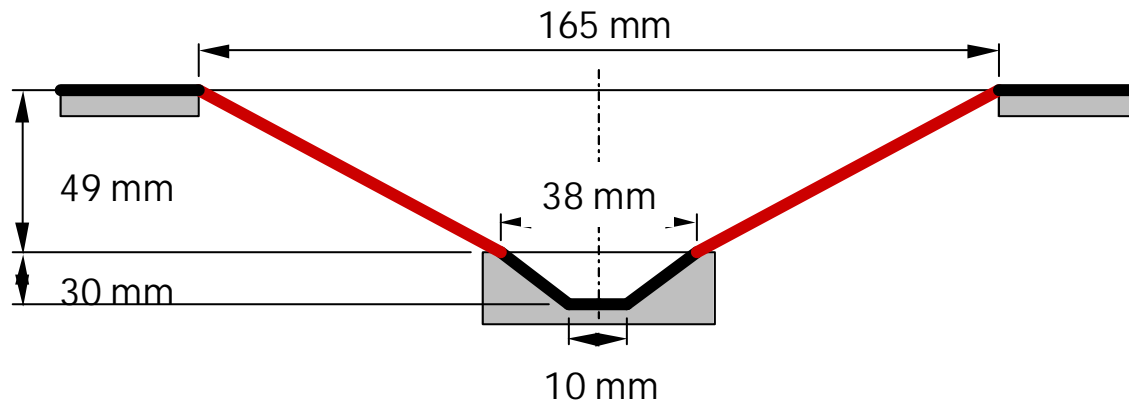
$$Z_{mr} \approx \frac{F}{v}$$

Mechanical Model

Radiation impedance

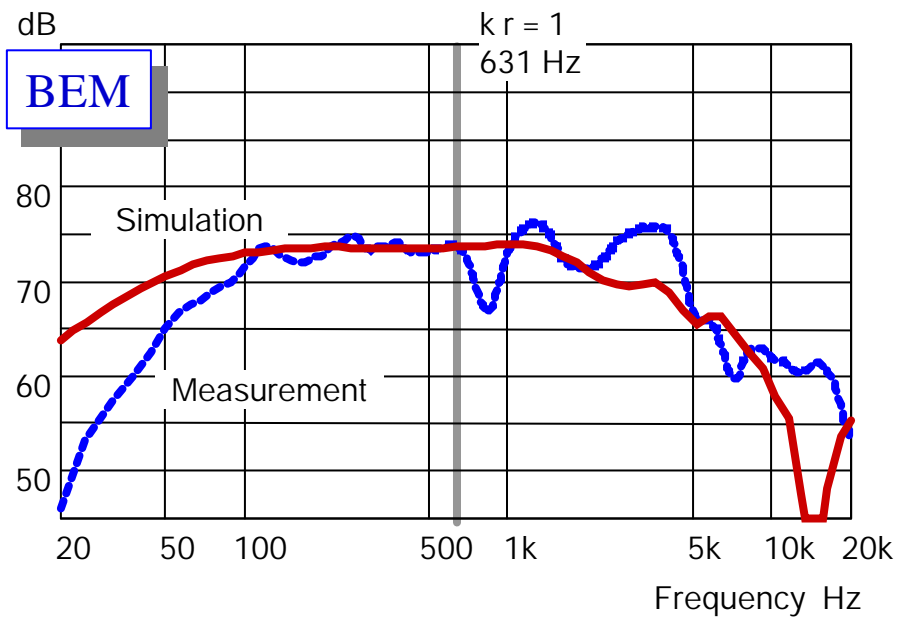
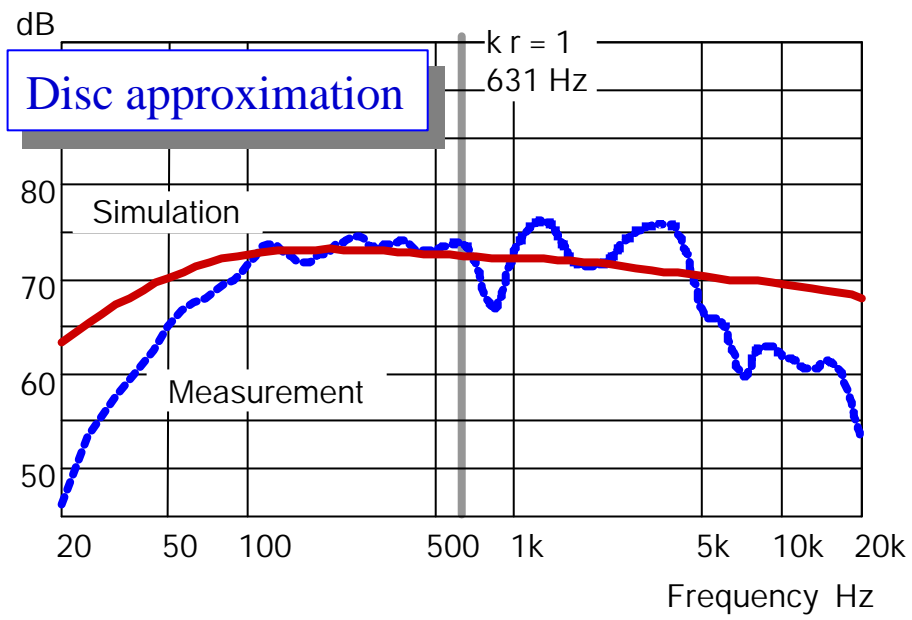
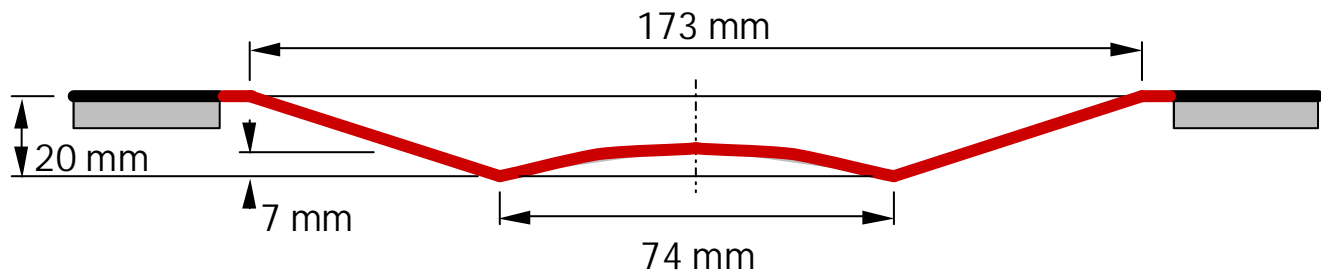


Sound Pressure Measurements



Far-field sound pressure on-axis

Sound Pressure Measurements



Far-field sound pressure on-axis

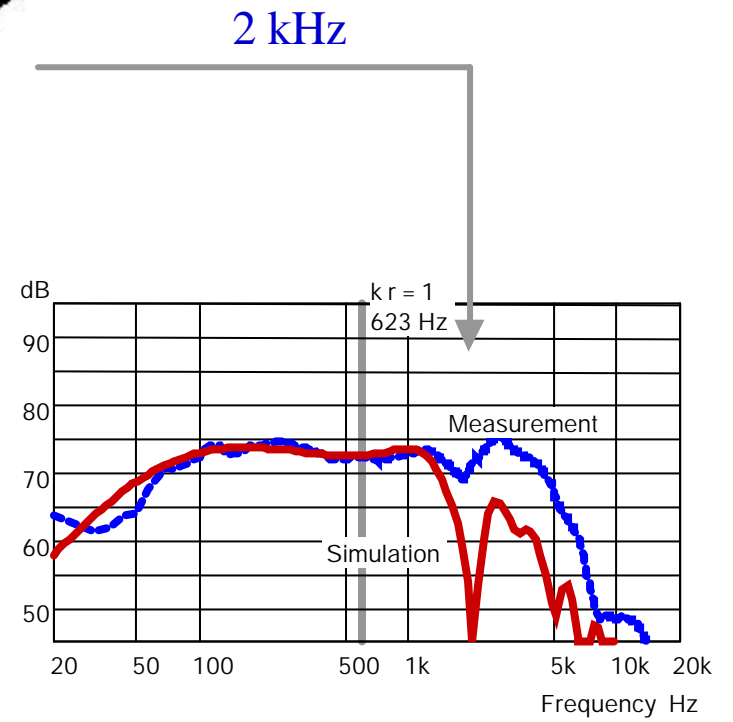
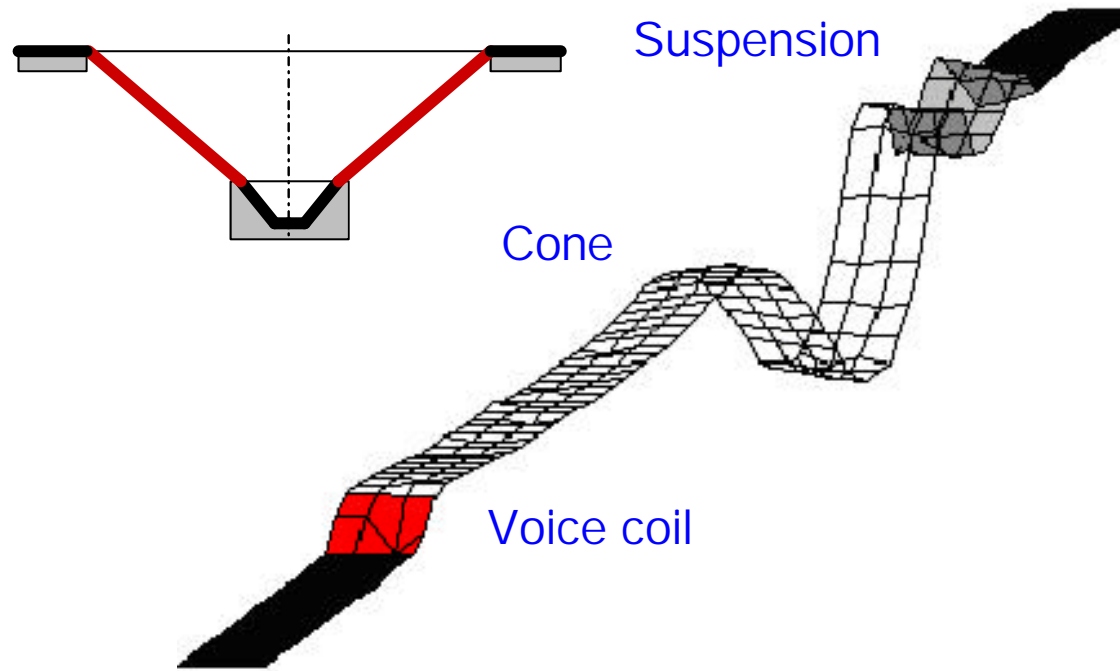
Sound Pressure Measurements

Rigid body model + BEM gives:

- One more octave of simulation bandwidth.
- Geometric data are needed additionally.
- Simulation bandwidth approx. $kr = 2 \dots 2.5$

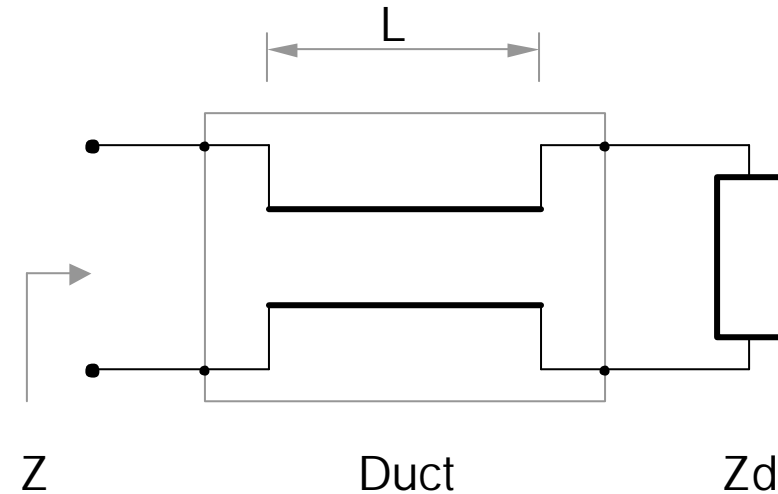
Sound Pressure Measurements

Membrane dynamics at 2 kHz



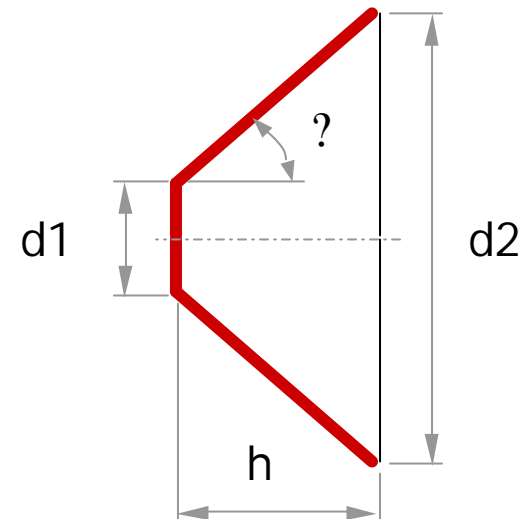
Approximation of Radiation Impedance

- Radiation impedance of rigid cone in infinite baffle.
- Approximation between disc model and BEM.
- Based on acoustic duct in fundamental mode.
- Duct loaded by radiation impedance Z_d of a disc with diameter d_2 in infinite baffle.

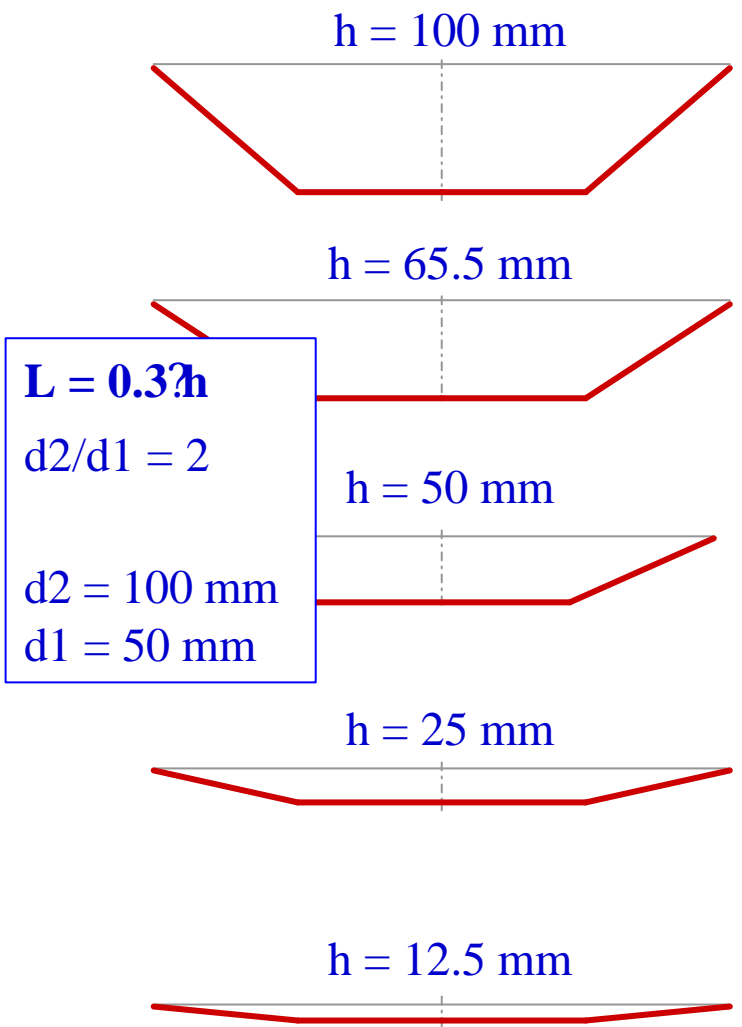


$$Z = \frac{Z_d \cos(kL) - i \sin(kL)}{\cos(kL) + i Z_d \sin(kL)}$$

$$L = \text{function} \left(h, \frac{d_2}{d_1} \right)$$

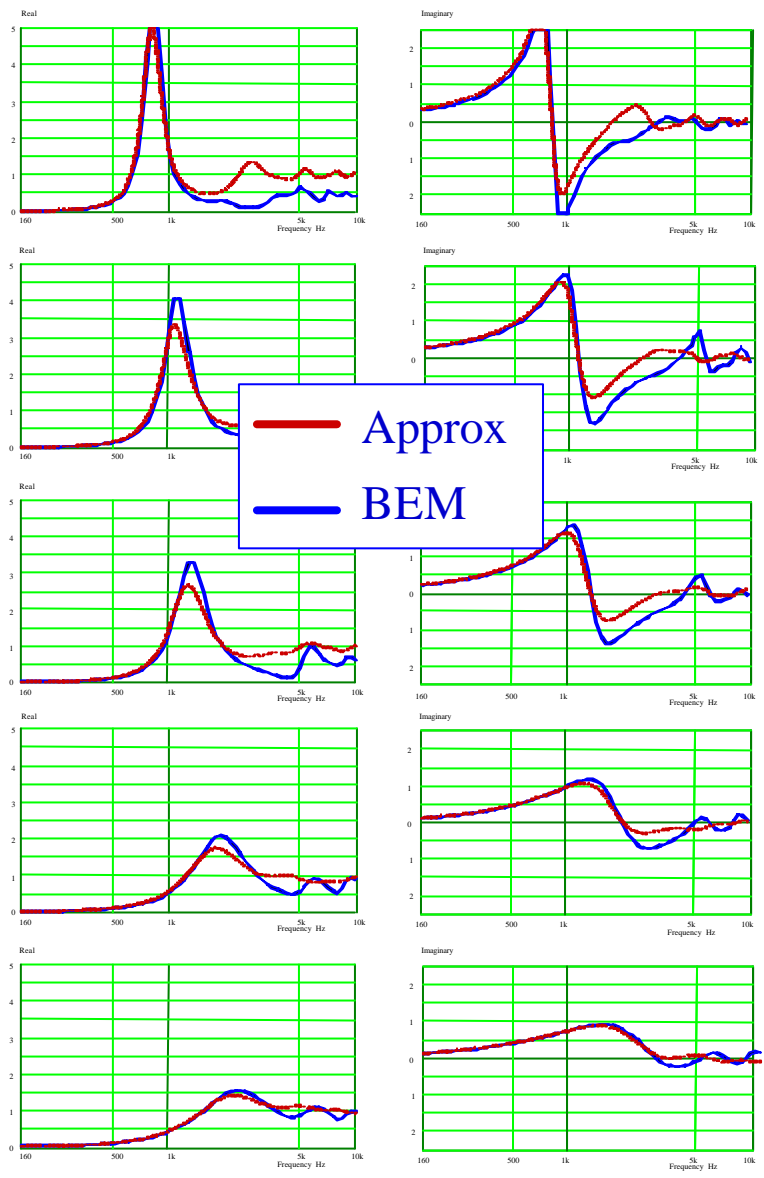


Approximation of Radiation Impedance

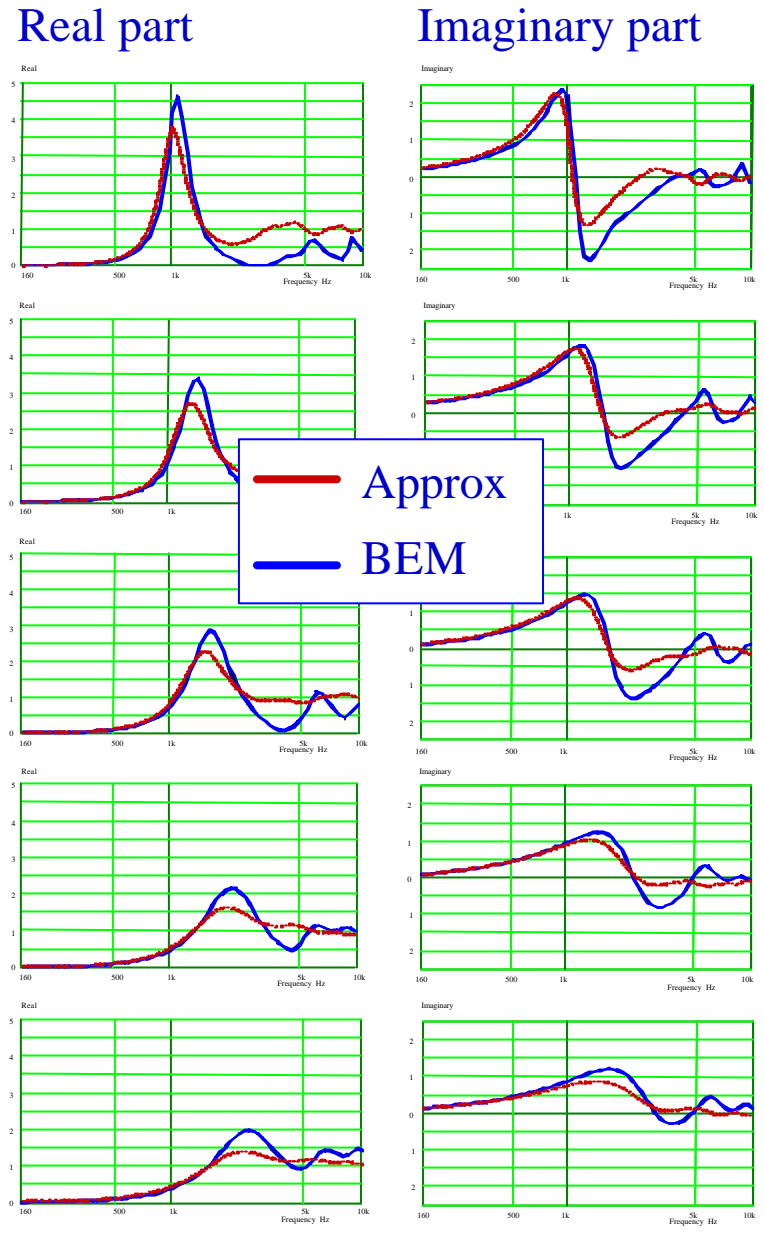
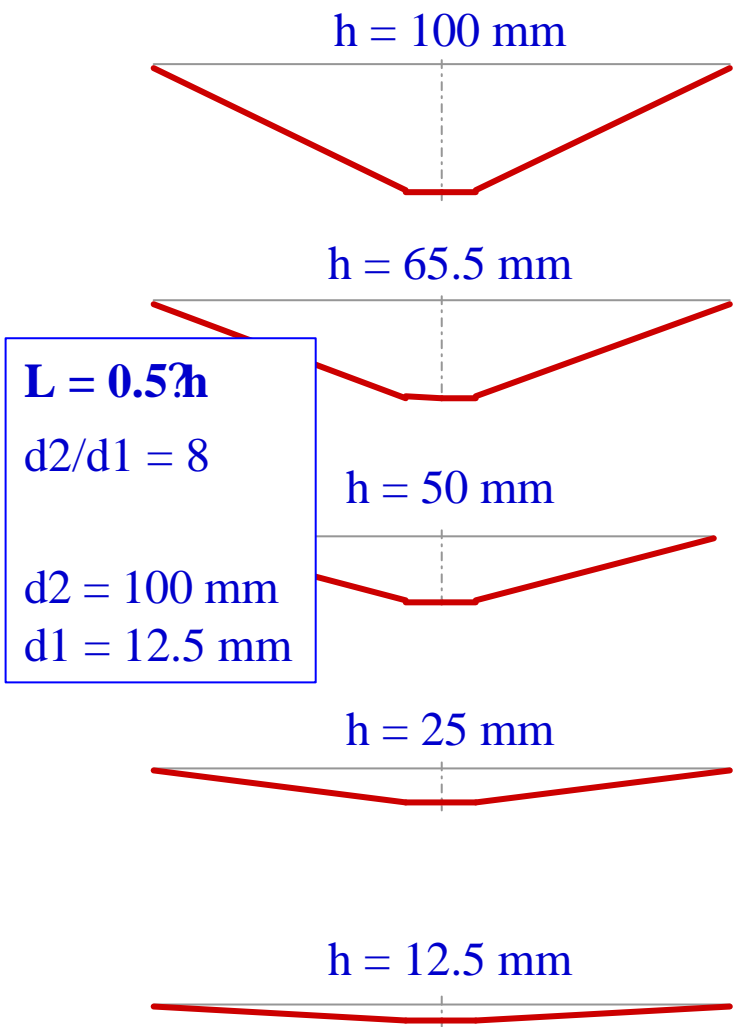


Real part

Imaginary part



Approximation of Radiation Impedance



Conclusions

- Application of BEM to radiation of cones
- Rigid body mode of mechanical system
- Confident model up to $k \cdot r = 2 \dots 2.5$
- Only geometrical data are necessary additionally
- Interesting approximation for radiation impedance of cones.
- Future work: Linking BEM to dynamical vibration of the cone

Thanks to NXT by supporting this research.
Special thanks to
Dr. Neil Harris, Dr. Graham Bank and Christien Ellis
for their help in analysis and measurements.

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"Radiation impedance of cones at high frequencies"

Joerg Panzer, NXT - New Transducers Ltd., U.K.